Joint IMD-WMO group fellowship Training On Numerical Weather Prediction By Meteorological Training Institute, India Meteorological Department (IMD), Pune

Atmospheric Boundary Layer (ABL) and its Parameterizations – Part II

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- Seemingly chaotic or random motion of fluid particles

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- Largest scales carry more Turbulence Kinetic Energy (TKE)
- Smallest scales carry much less TKE

 $\tilde{a}(\mathbf{x}, t) = A(\mathbf{x}, t) + a(\mathbf{x}, t)$

Mean

Instantaneous

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 $\frac{\partial \tilde{u}_i}{\partial x_i} = \frac{\partial (U_i + u_i)}{\partial x_i} = 0$

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Overbar denotes averaging operation

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\end{array}$$

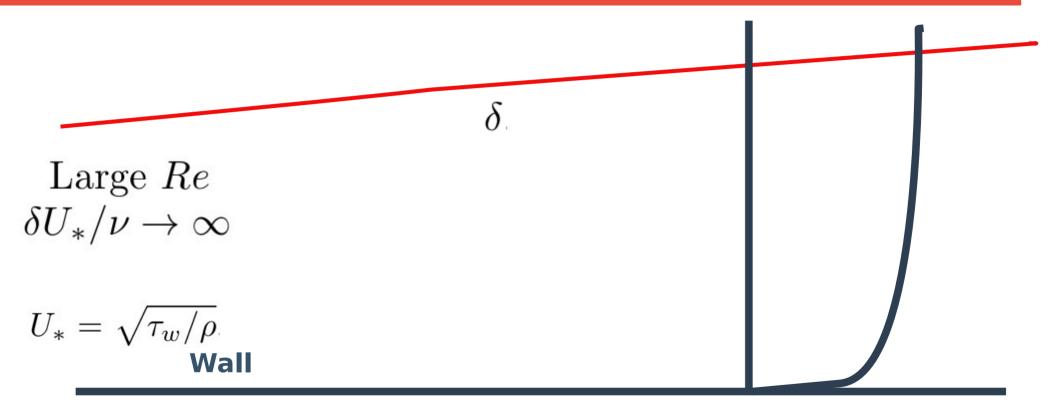
2. Turbulence Equations: Mean Flow Kinetic Energy

Time rate of change = flux divergence + pressure gradient work - viscous dissipation - loss to turbulence

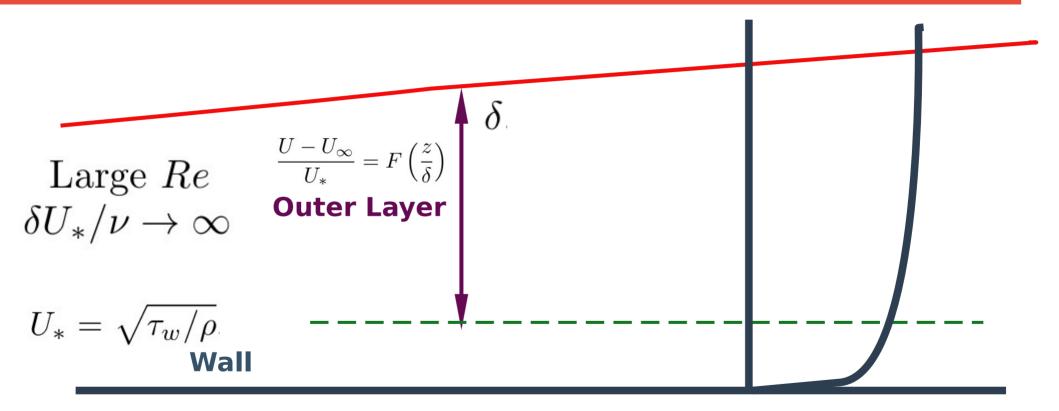
2. Turbulence Equations: TKE

$$\frac{1}{2}\frac{\partial}{\partial t}\overline{u_{i}u_{i}} = -\frac{U_{j}}{2}\frac{\partial}{\partial x_{j}}\overline{u_{i}u_{i}} - \overline{u_{i}u_{j}}\frac{\partial U_{i}}{\partial x_{j}} - \frac{1}{2}\frac{\partial}{\partial x_{j}}\overline{u_{i}u_{i}u_{j}}$$
$$-\frac{1}{\rho}\frac{\partial}{\partial x_{i}}\overline{pu_{i}} - \nu\frac{\overline{\partial u_{i}}}{\partial x_{j}}\frac{\partial u_{i}}{\partial x_{j}}.$$

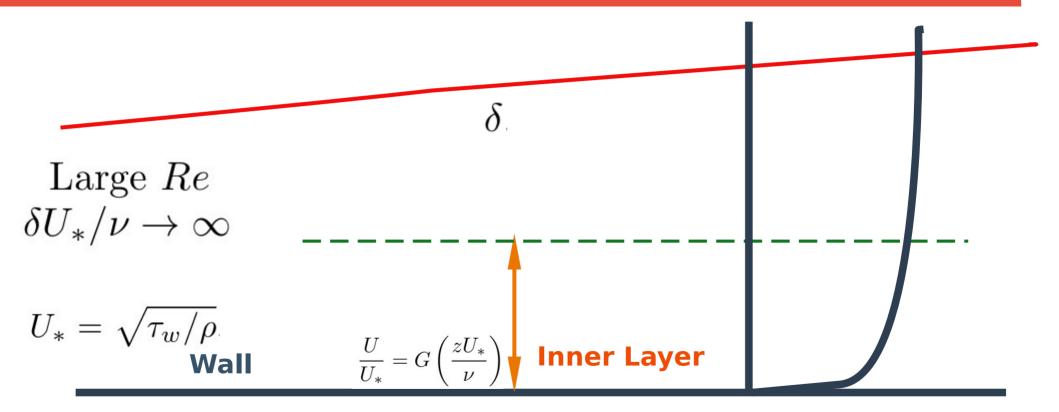
Time rate of change = advective divergence + gain from mean flow + pressure and flux divergence + viscous dissipation

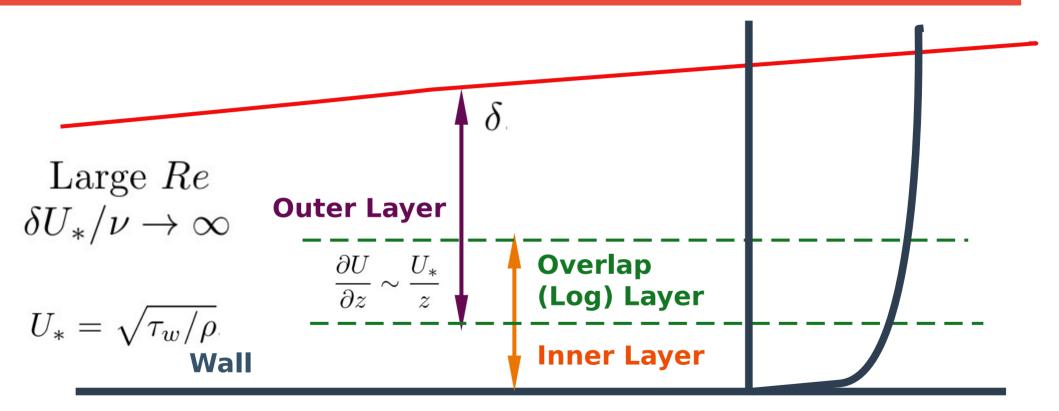


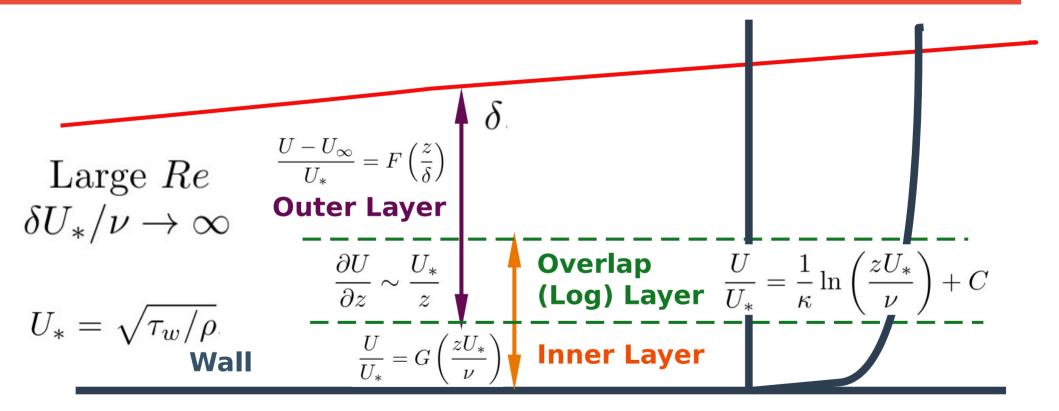




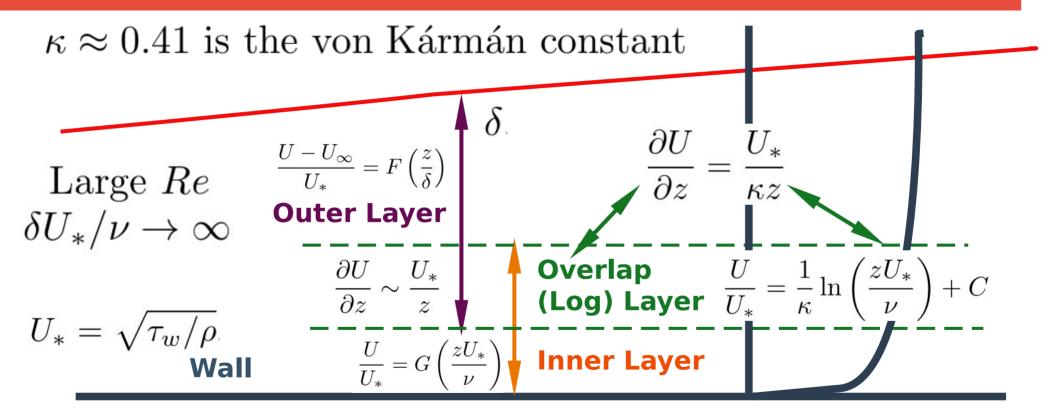














Hydrostatic "Background" OR "Base" State

 $p_0 = \rho_0 R_d T_0$ Eqn. of thermodynamic state

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- $rac{dp_0}{dx_3}
 ho_0 g = 0$ Mom. Eqn for steady, motionless atmosphere

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 $T\frac{Ds}{Dt} = \frac{Dh}{Dt} - \frac{1}{\rho}\frac{Dp}{Dt} \ ^{\rm 2nd} \ {\rm law \ of \ thermodynamics} \label{eq:Tdef}$

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, so that $\frac{Dh_0}{Dt} = \frac{1}{\rho_0} \frac{Dp_0}{Dt}$

Isentropic, imaginary displacements of fluid parcel in the vertical direction

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|--------|---|----------|--------|
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 2nd law of thermodynamics

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Isentropic, imaginary displacements of fluid parcel in the vertical direction

$$\frac{dh_0}{dx_3} = \frac{1}{\rho_0} \frac{dp_0}{dx_3}$$
$$h_0 = c_p T_0$$
$$\frac{dT_0}{dx_3} = -\frac{g}{c_p}$$

Base state vertical variation of enthalpy and temperature

Flow-Induced "Small" Perturbations Around the "Base" State

$$\tilde{p} = p_0(z) + \tilde{p}'(\mathbf{x}, t); \qquad \tilde{T} = T_0(z) + \tilde{T}'(\mathbf{x}, t); \qquad \tilde{\rho} = \rho_0(z) + \tilde{\rho}'(\mathbf{x}, t)$$

Flow-Induced "Small" Perturbations Around the "Base" State

$$\begin{split} \tilde{p} &= p_0(z) + \tilde{p}'(\mathbf{x}, t); \qquad \tilde{T} = T_0(z) + \tilde{T}'(\mathbf{x}, t); \qquad \tilde{\rho} = \rho_0(z) + \tilde{\rho}'(\mathbf{x}, t) \\ \tilde{\rho}' &= \tilde{\rho}'(\tilde{T}, \tilde{p}) \simeq \frac{\partial \rho}{\partial T} \Big|_0 \tilde{T}' + \frac{\partial \rho}{\partial p} \Big|_0 \tilde{p}' \\ &= -\frac{\rho_0}{T_0} \tilde{T}' + \frac{1}{R_{\rm d} T_0} \tilde{p}'. \end{split}$$

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$$\tilde{\rho}' &= -\frac{\rho_0}{T_0} \tilde{T}'. \end{split}$$

Density fluctuation is proportional to temperature fluctuation

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$$\begin{split} \tilde{T} &= T_0(z) + \tilde{T}'(\mathbf{x}, t); \qquad \tilde{\rho} = \rho_0(z) + \tilde{\rho}'(\mathbf{x}, t) \\ \frac{\partial \tilde{\rho}}{\partial t} + \frac{\partial \tilde{\rho} \tilde{u}_i}{\partial x_i} = \frac{D \tilde{\rho}}{Dt} + \tilde{\rho} \frac{\partial \tilde{u}_i}{\partial x_i} = 0 \\ \tilde{u}_3 \frac{d \rho_0}{d x_3} + \rho_0 \frac{\partial \tilde{u}_i}{\partial x_i} \simeq 0, \qquad \text{Mass Conservatio n Eqn.} \end{split}$$

Density fluctuation is proportional to temperature fluctuation

Flow-Induced "Small" Perturbations Around the "Base" State

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$$\begin{split} &\stackrel{\tilde{T}}{=} T_0(z) + \tilde{T}'(\mathbf{x}, t); \qquad \tilde{\rho} = \rho_0(z) + \tilde{\rho}'(\mathbf{x}, t) \\ &\stackrel{\tilde{\theta}}{=} \frac{\partial \tilde{\rho}}{\partial t} + \frac{\partial \tilde{\rho} \tilde{u}_i}{\partial x_i} = \frac{D \tilde{\rho}}{Dt} + \tilde{\rho} \frac{\partial \tilde{u}_i}{\partial x_i} = 0 \\ &\stackrel{\tilde{u}_3}{\tilde{d} \frac{d \rho_0}{d x_3}} + \rho_0 \frac{\partial \tilde{u}_i}{\partial x_i} \simeq 0, \qquad \begin{array}{c} \text{Mass} \\ \text{Conservatio} \\ n \text{ Eqn.} \\ &\stackrel{\tilde{\theta}}{\tilde{u}_i} \simeq -\frac{\tilde{u}_3}{\rho_0} \frac{d \rho_0}{d x_3} = \frac{\tilde{u}_3}{H_\rho} \end{split}$$

Density fluctuation is proportional to temperature fluctuation

If boundary layer height << Hp, then divergence can be assumed to be negligible

Final set of dry-air Instantaneous Equations

 $\frac{\partial \tilde{u}_i}{\partial x_i} = 0$

Mass Conservation

Final set of dry-air Instantaneous Equations

$$\frac{\partial \tilde{u}_i}{\partial x_i} = 0 \qquad \qquad \frac{\partial \tilde{u}_i}{\partial t} + \tilde{u}_j \frac{\partial \tilde{u}_i}{\partial x_j} = -\frac{1}{\rho_0} \frac{\partial \tilde{p}'}{\partial x_i} - 2\epsilon_{ijk} \Omega_j \tilde{u}_k + \frac{g}{\theta_0} \tilde{\theta}' \delta_{3i} + \nu \nabla^2 \tilde{u}_i$$

Mass Conservation

Momentum Equation

Final set of dry-air Instantaneous Equations

$$\frac{\partial \tilde{u}_i}{\partial x_i} = 0 \qquad \qquad \frac{\partial \tilde{u}_i}{\partial t} + \tilde{u}_j \frac{\partial \tilde{u}_i}{\partial x_j} = -\frac{1}{\rho_0} \frac{\partial \tilde{p}'}{\partial x_i} - 2\epsilon_{ijk}\Omega_j \tilde{u}_k + \frac{g}{\theta_0} \tilde{\theta}' \delta_{3i} + \nu \nabla^2 \tilde{u}_i$$

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Mass Conservation

Momentum Equation

$$\frac{\partial \tilde{\theta}}{\partial t} + \tilde{u}_i \frac{\partial \tilde{\theta}}{\partial x_i} = \alpha \nabla^2 \tilde{\theta} - \frac{\tilde{\theta}}{\rho c_p \tilde{T}} \frac{\partial \tilde{R}_i}{\partial x_i}$$

Thermal Energy Equation

Final set of dry-air Instantaneous Equations

$$\frac{\partial \tilde{u}_i}{\partial x_i} = 0 \qquad \qquad \frac{\partial \tilde{u}_i}{\partial t} + \tilde{u}_j \frac{\partial \tilde{u}_i}{\partial x_j} = -\frac{1}{\rho_0} \frac{\partial \tilde{p}'}{\partial x_i} - 2\epsilon_{ijk}\Omega_j \tilde{u}_k + \frac{g}{\theta_0} \tilde{\theta}' \delta_{3i} + \nu \nabla^2 \tilde{u}_i$$

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Mass Conservation

Momentum Equation

$$\frac{\partial \tilde{\theta}}{\partial t} + \tilde{u}_i \frac{\partial \tilde{\theta}}{\partial x_i} = \alpha \nabla^2 \tilde{\theta} - \frac{\tilde{\theta}}{\rho c_p \tilde{T}} \frac{\partial \tilde{R}_i}{\partial x_i}$$

Thermal Energy Equation

"Passive" Scalar Conservation Equation

 $\frac{\partial \tilde{c}}{\partial t} + \tilde{u}_i \frac{\partial \tilde{c}}{\partial x_i} = \gamma \frac{\partial^2 \tilde{c}}{\partial x_i \partial x_i}$



Final set of moist-air Instantaneous Equations

$$\begin{aligned} \frac{\partial \tilde{u}_i}{\partial t} + \tilde{u}_j \frac{\partial \tilde{u}_i}{\partial x_j} &= -\frac{1}{\rho_0} \frac{\partial \tilde{p}'}{\partial x_i} - 2\epsilon_{ijk} \Omega_j \tilde{u}_k + \frac{g}{\theta_0} \tilde{\theta}_v' \delta_{3i} + \nu \nabla^2 \tilde{u}_i \\ \frac{\partial \tilde{u}_i}{\partial x_i} &= 0, \\ \frac{\partial \tilde{\theta}}{\partial t} + \tilde{u}_j \frac{\partial \tilde{\theta}}{\partial x_j} &= \alpha \nabla^2 \tilde{\theta} - \frac{\tilde{\theta}}{\rho_0 c_p \tilde{T}} \frac{\partial \tilde{R}_j}{\partial x_j}, \\ \frac{\partial \tilde{q}}{\partial t} + \tilde{u}_i \frac{\partial \tilde{q}}{\partial x_i} &= \gamma \frac{\partial^2 \tilde{q}}{\partial x_i \partial x_i}. \end{aligned}$$

Final set of moist-air Averaged Equations

$$\begin{split} \tilde{u}_i &= U_i + u_i, \qquad \tilde{p}' = P + p, \qquad \tilde{\theta}'_{\rm v} = \Theta'_{\rm v} + \theta_{\rm v}, \\ \frac{\tilde{\theta}}{\rho_0 c_p \tilde{T}} \frac{\partial \tilde{R}_i}{\partial x_i} &= \mathcal{R} + r, \qquad \tilde{c} = C + c, \qquad \tilde{\theta} = \Theta + \theta. \end{split}$$

Final set of moist-air Averaged Equations

$$\frac{\partial U_i}{\partial t} + U_j \frac{\partial U_i}{\partial x_j} + \frac{\partial}{\partial x_j} \overline{u_i u_j} = -\frac{1}{\rho_0} \frac{\partial P}{\partial x_i} - 2\epsilon_{ijk} \Omega_j U_k + \frac{g}{\theta_0} \Theta'_v \delta_{3i},$$
$$\frac{\partial U_i}{\partial x_i} = 0.$$
$$\frac{\partial \Theta}{\partial t} + U_i \frac{\partial \Theta}{\partial x_i} + \frac{\partial \overline{\partial u_i}}{\partial x_i} + \mathcal{R} = 0,$$
$$\frac{\partial C}{\partial t} + U_i \frac{\partial C}{\partial x_i} + \frac{\partial \overline{c u_i}}{\partial x_i} = 0.$$
Mean Flow

Final set of moist-air Averaged Equations

$$\frac{\partial \overline{u_i u_k}}{\partial t} + U_j \frac{\partial \overline{u_i u_k}}{\partial x_j} = -\overline{u_j u_k} \frac{\partial U_i}{\partial x_j} - \overline{u_j u_i} \frac{\partial U_k}{\partial x_j} \text{ (mean-gradient production)} - 2\epsilon_{ijm}\Omega_j \overline{u_m u_k} - 2\epsilon_{kjm}\Omega_j \overline{u_m u_i} \text{ (Coriolis)} + \frac{g}{\theta_0} \left(\overline{\theta_v u_k} \delta_{3i} + \overline{\theta_v u_i} \delta_{3k} \right) \text{ (buoyant production)} - \frac{1}{\rho_0} \left(\overline{u_k} \frac{\partial p}{\partial x_i} + \overline{u_i} \frac{\partial p}{\partial x_k} \right) \text{ (pressure-gradient interaction)} - \frac{2\epsilon}{3} \delta_{ik} \text{ (viscous dissipation).}$$

Reynolds Stresses